

**Lecture Notes**

**Electrical Machines IV**

**Code: CECE437**

**Level: Four**

**Points: 100 = 25+15+60**

## **Course Contents**

- **Three phase induction motors:**
  - Introduction.
  - Advantages and disadvantages.
  - Construction.
  - Rotating magnetic field due to 3-phase currents.
  - Principle of operation.
  - Slip, Rotating current frequency, Effect of the slip on the rotor current.
  - Rotor current, Rotor Torque.
  - Starting torque, Condition for maximum starting torque.
  - Effect of change of supply voltage.
  - Motor under load.
  - Torque under running condition.
  - Maximum torque under running conditions.
  - Torque-Slip characteristics.
  - Comparison between transformer and Induction motor.
  - Speed regulation of induction motor.
  - Speed control of induction motor.

## **Course Contents ...**

- Power factor & Power stages in induction motor.
- Equivalent circuit of 3-phase induction motor.
- Induction motor ratings.
- **Single phase induction motor:**
  - Self-starting.
  - Capacitor start motor.
  - Equivalent circuit of 1-phase induction motor.
- **Testing methods of three phase induction motor.**

## Introduction

- The 3-ph induction motors, the most widely used in industry.
- They run at essentially constant speed from no load to full load.
- We usually prefer DC motors when large speed variations are required.

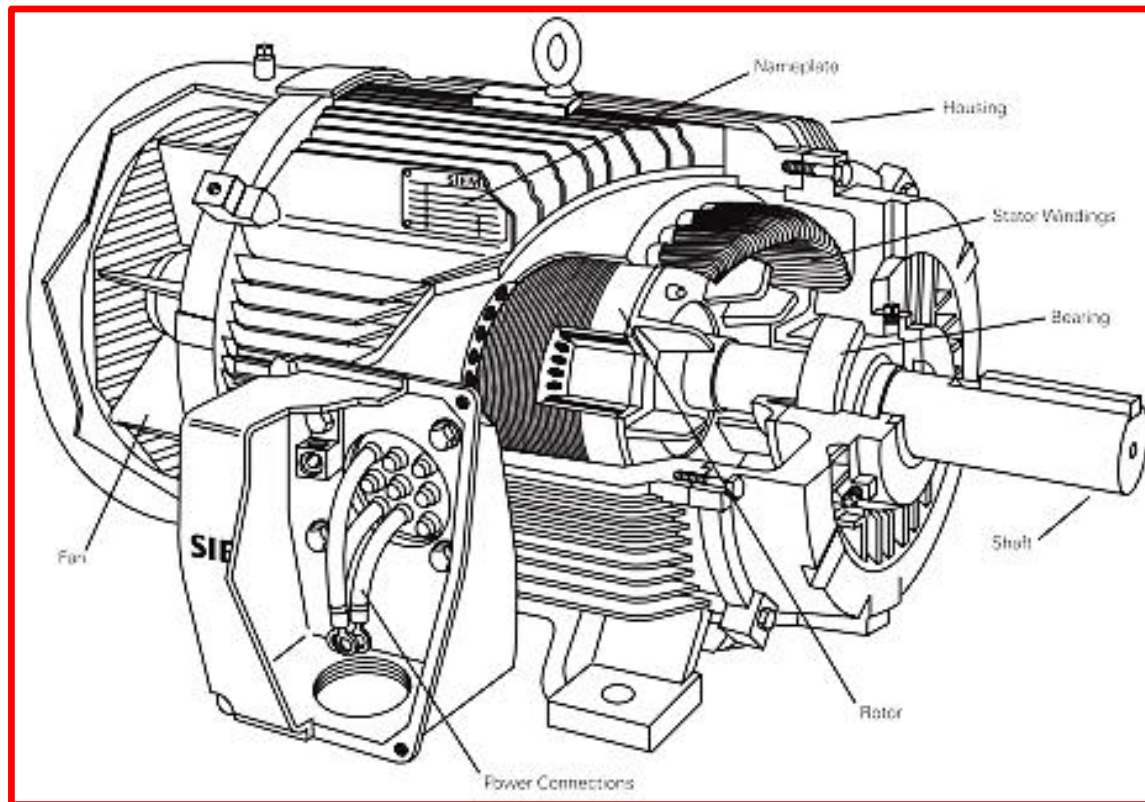


Fig: three phase induction motor

## **Advantages of 3-phase Induction Motors**

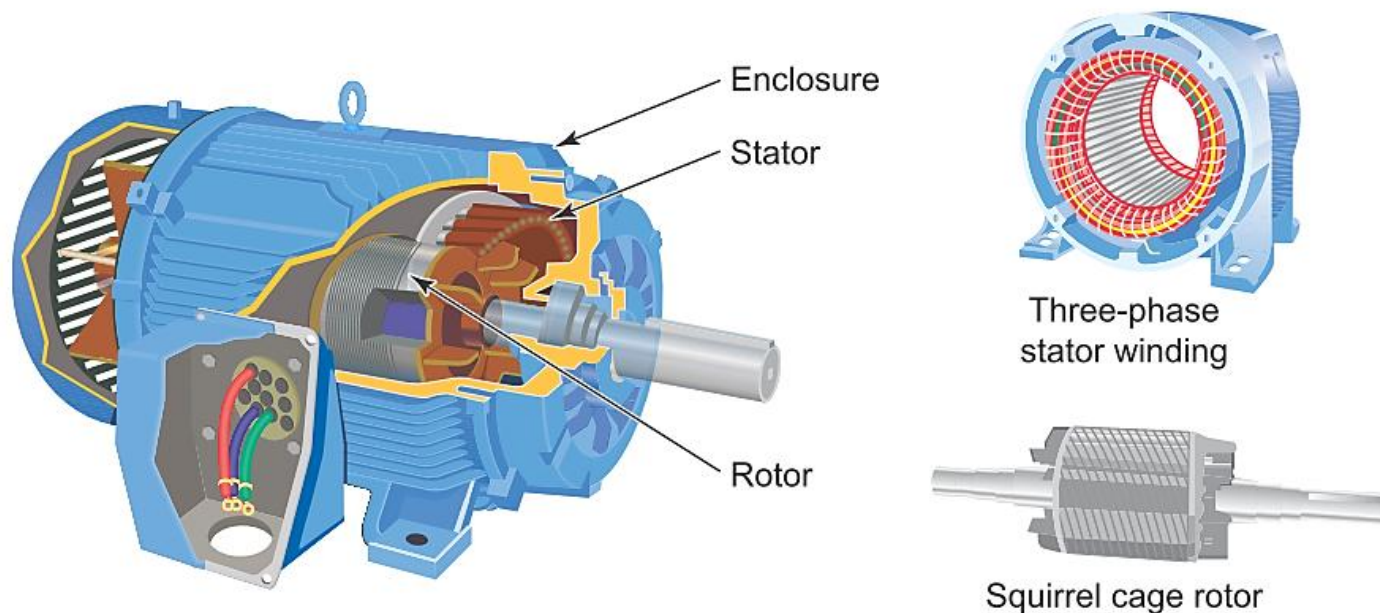
- It has simple and rugged construction.
- It is relatively cheap.
- It requires little maintenance.
- It has high efficiency and good power factor.
- It has self-starting torque.

## **Disadvantages of 3-phase Induction Motors**

- It is essentially has a constant speed and its speed cannot be changed easily.
- Its starting torque is less than that of DC motors.

## Construction of 3-phase Induction Motors

- It has two main parts: (i) **Stator**: the stationary part.  
(ii) **Rotor**: the rotating part.
- There is a small air gap between the rotor and stator (0.4 mm to 4 mm) depend on the power of the motor.



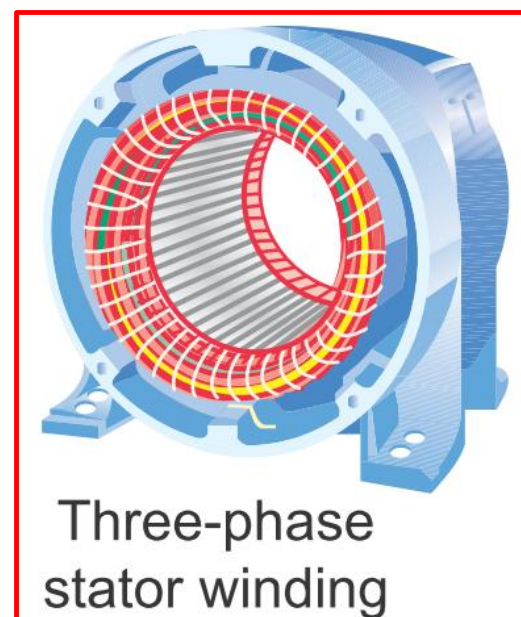
**Figure 5-35** Squirrel-cage induction motor.

Fig. 1: Three phase squirrel cage induction motor

## Construction of 3-phase Induction Motors ...

### (i) Stator:

- A hollow cylindrical core made up of thin silicon steel laminations to reduce the hysteresis and eddy current losses.
- Has an even number of slots on the inner periphery.
- Has 3-phase stator windings put in the slots to form Y or  $\Delta$  connected circuit. The windings configuration determines the number of poles in the induction motor.
- As number of poles decreases, the motor speed increases and vice versa.
- When the 3-phase windings are energized from a 3-phase supply, a rotating magnetic field of constant magnitude is produced. This rotating field induces currents in the rotor by means of electromagnetic induction, then, the rotor rotates.



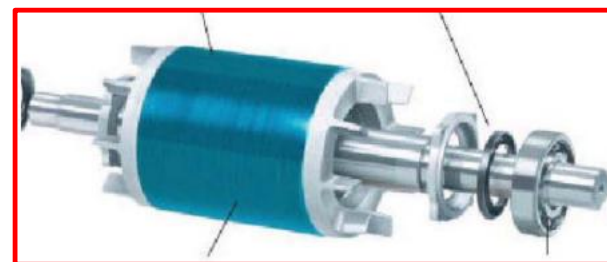
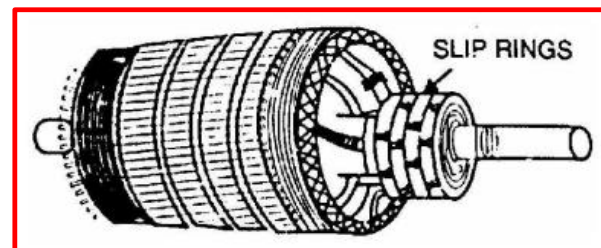
## Construction of 3-phase Induction Motors ...

### (ii) Rotor:

- A steel laminated core mounted on a shaft. It has slots on its outer periphery, a 3-phase windings are placed in these slots.
- It has two types: [A] Squirrel cage rotor القفص السنجابي  
[B] Wound rotor ملفوف

### [A] Squirrel cage rotor type:

- A laminated cylindrical core having slots on outer periphery, each slot has one bar of AL or Cu bar. These bars are short-circuited at each end by means of slip rings. “hence the name is squirrel cage”
- Not connected to a 3-phase supply, but having currents induced in it by means of electromagnetic induction.
- Simple and rugged construction.
- Low starting torque: (*Why*) {Because: the rotor bars are permanently short-circuited and it is not possible to add any external resistance to the rotor circuit to give a large starting torque}.

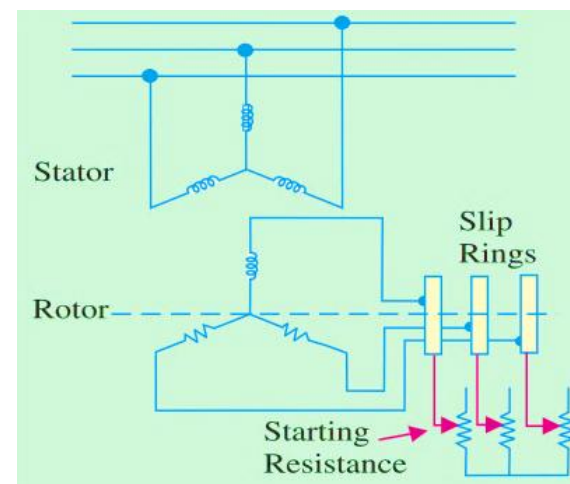
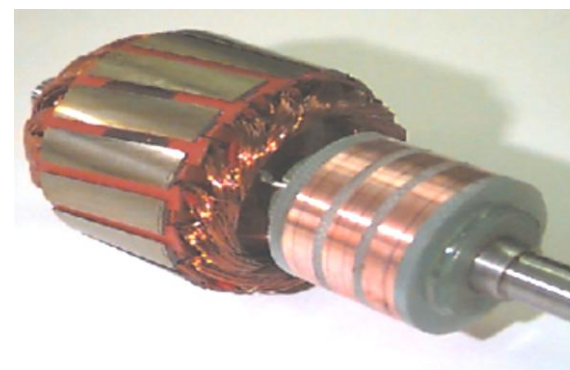




## - Construction of 3-phase Induction Motors ...

### [B] Wound rotor type:

- A laminated cylindrical core having slots on outer periphery to carry 3-phase windings “Y-connected”.
- The open end of the 3-phase windings are jointed to insulated slip rings mounted on the rotor shaft with one brush resting on each slip ring.
- The brushes are connected to a 3-phase Y-connected rheostat.
- Has large starting torque. (*Why*) {Because: at starting, the external resistances are included in the rotor circuit to give high starting torque. These resistances are gradually reduced to zero as the motor runs up to the required speed}.



When the motor reach the normal speed; the external resistances are short-circuited, so that the wound rotor runs like a squirrel cage type.

## Rotating Magnetic Field Due to 3-phase Currents

- When the 3-phase **stator** winding are energized from a 3-phase supply, a rotating magnetic field is produced, and this field has poles goes on shifting their positions around the stator.
- For the reason of rotation, it is called “*a rotating magnetic field*”.
- **(Magnitude of rotating field) = 1.5 \* (Maximum flux due to any phase)**  
$$= 1.5 * \phi_m$$

## How the rotating magnetic field is produced?

**Answer:** consider a 2-pole, 3-phase winding as shown in Fig. 6. The three phases of the stator X, Y and Z are energized from a 3-phase source and currents in these phases are  $I_x$ ,  $I_y$  and  $I_z$ .

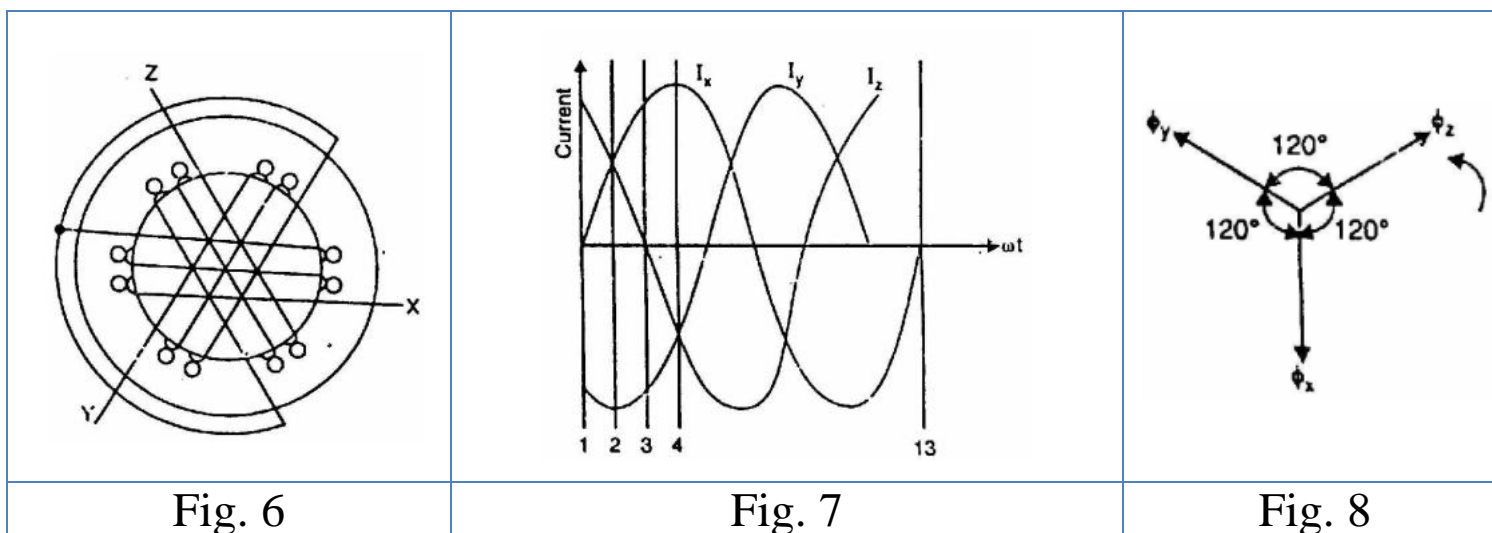
- Referring to Fig. 7, the fluxes by these currents are given by:

$$\phi_x = \phi_m \sin \omega t$$

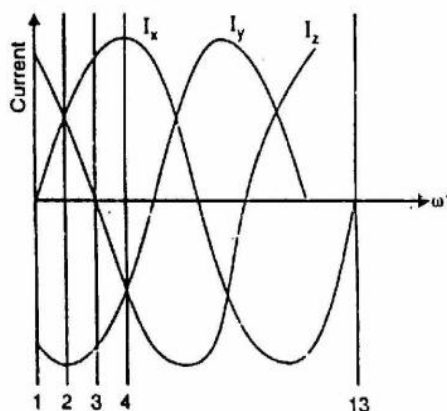
$$\phi_y = \phi_m \sin (\omega t - 120^\circ)$$

$$\phi_z = \phi_m \sin (\omega t - 240^\circ)$$

- Fig. 8 shows the phasor diagram of the three phase fluxes.



- We shall now prove that this 3-phase supply produces a rotating field of constant magnitude equal to  $1.5\Phi_m$ .



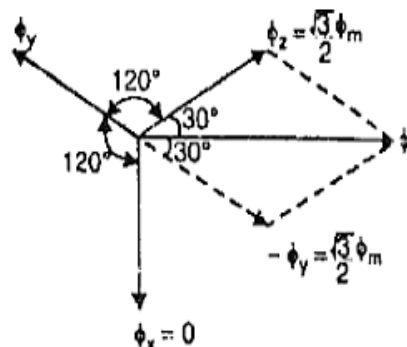
For position no. 1 in Fig.7: [ $I_x=0$ ,  $I_y$  and  $I_z$  are equal and opposite]. This establishes a flux as shown in Fig 9.1.

at  $\omega t = 0$ ;

$$\phi_x = 0$$

$$\phi_y = \phi_m \sin(-120^\circ) = -\frac{\sqrt{3}}{2} \phi_m$$

$$\phi_z = \phi_m \sin(-240^\circ) = \frac{\sqrt{3}}{2} \phi_m$$



$$\text{Resultant flux, } \phi_r = 2 \times \frac{\sqrt{3}}{2} \phi_m \cos \frac{60^\circ}{2} = 2 \times \frac{\sqrt{3}}{2} \phi_m \times \frac{\sqrt{3}}{2} = 1.5 \phi_m$$

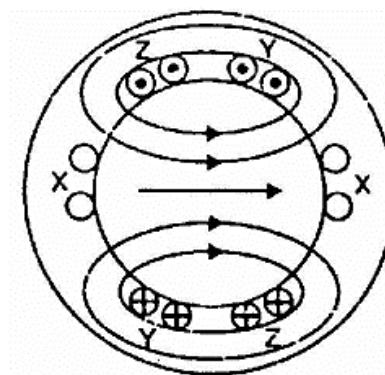
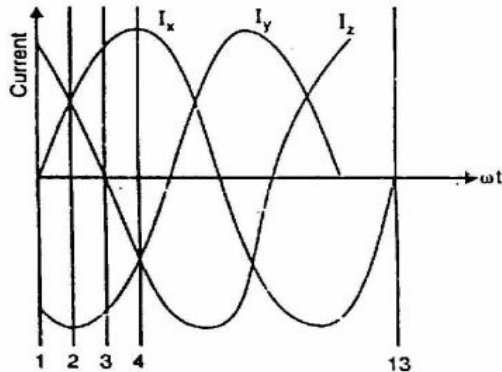


Fig. 9.1



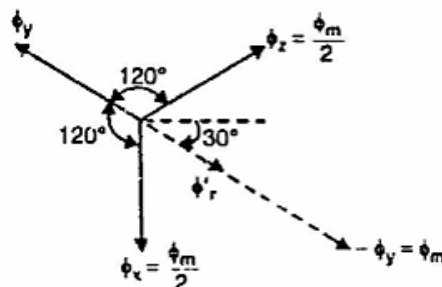
For position no. 2 in Fig.7: The current is maximum (negative) in  $\phi_y$  phase Y and 0.5 maximum (positive) in phases X and Z. This establishes a flux as shown in Fig 9.2.

at  $\omega t = 30^\circ$ ;

$$\phi_x = \phi_m \sin 30^\circ = \frac{\phi_m}{2}$$

$$\phi_y = \phi_m \sin(-90^\circ) = -\phi_m$$

$$\phi_z = \phi_m \sin(-210^\circ) = \frac{\phi_m}{2}$$



Phasor sum of  $\phi_x$  and  $\phi_z$   $\longrightarrow$   $\phi'_r = 2 \times \frac{\phi_m}{2} \cos \frac{120^\circ}{2} = \frac{\phi_m}{2}$

Phasor sum of  $\phi'_r$  and  $-\phi_y$   $\longrightarrow$   $\phi_r = \frac{\phi_m}{2} + \phi_m = 1.5 \phi_m$

Note that resultant flux is displaced  $30^\circ$  clockwise from position 1.

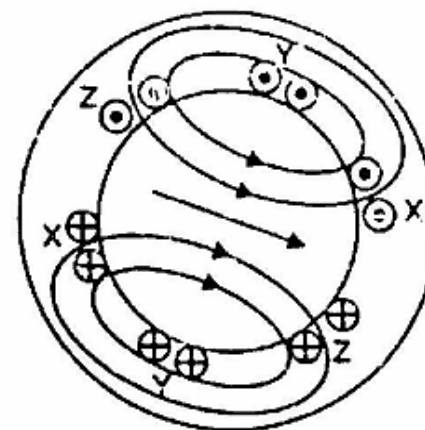
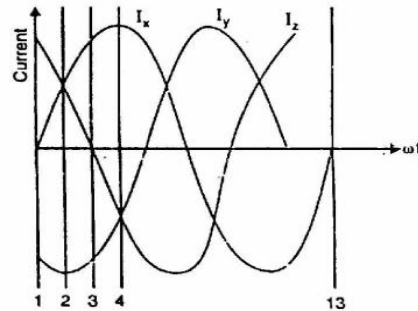


Fig. 9.2



For position no. 3 in Fig.7: current in phase Z is zero and the currents in phases X and Y are equal and opposite (currents in phases X and Y are  $0.866 \times$  max. value). This establishes a flux as shown in Fig 9.3.

at  $\omega t = 60^\circ$ ;

$$\phi_x = \phi_m \sin 60^\circ = \frac{\sqrt{3}}{2} \phi_m;$$

$$\phi_y = \phi_m \sin(-60^\circ) = -\frac{\sqrt{3}}{2} \phi_m$$

$$\phi_z = \phi_m \sin(-180^\circ) = 0$$

$$\phi_r = 2 \times \frac{\sqrt{3}}{2} \phi_m \cos \frac{60^\circ}{2} = 1.5 \phi_m$$

Note that resultant flux is displaced  $60^\circ$  clockwise from position 1.

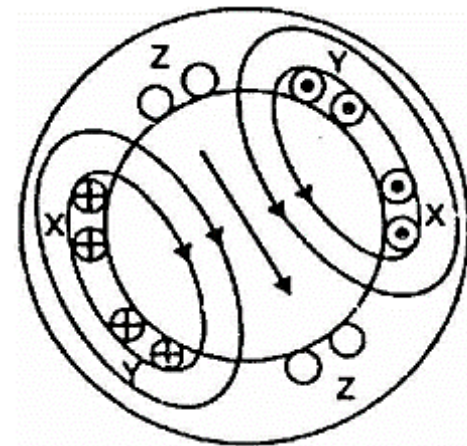
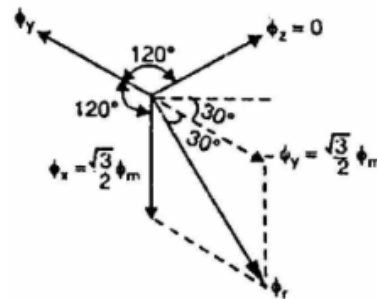


Fig. 9.3

And so on... ■

